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High-speed and high-sensitivity parallel spectraldomain optical coherence tomography using a supercontinuum light source

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The three most important metrics in optical coherence tomography (OCT) are resolution, speed, and sensitivity. Because there is a complex interplay between these metrics, no previous work has obtained the best performance in all three metrics simultaneously. We demonstrate that a high-power supercontinuum source, in combination with parallel spectral-domain OCT, achieves an unparalleled combination of resolution, speed, and sensitivity. This system captures cross-sectional images spanning 4 mm × 0.5 mm at 1,024,000 lines/s with $2 \times 14 \,\mu\text{m}$ resolution (axial × transverse) at a sensitivity of 113 dB. Imaging using the proposed system is demonstrated on highly differentiated human bronchial epithelial cells to capture and spatially localize ciliary dynamics. © 2016 Optical Society of America

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Optical coherence tomography (OCT) has become one of the most effective imaging modalities for performing noninvasive, real-time biological imaging. The three most important metrics for OCT are resolution, speed, and sensitivity. However, all three cannot be limitlessly improved because they are subject to trade-offs. High speed is necessary for capturing rapid dynamics of biological processes and transient responses to external perturbations. The highest speed system reported to date is a swept-source OCT (SS-OCT) system with a line rate of 40 MHz (megahertz) [1]. But, to our knowledge, no SS-OCT system has been reported that combines MHz A-line rates with the bandwidth necessary for ultrahigh resolution (<3 axial μ m). Spectral-domain OCT (SD-OCT) systems use broad bandwidth sources to achieve axial resolutions as

low as 1 μ m [2]. The highest speed SD-OCT system has a line rate of 1 million A-lines/sec, but offers only a modest sensitivity of 72 dB [3].

Importantly, all high-speed OCT systems are subject to a trade-off between sensitivity and speed because of limited exposure time in order to scan rapidly. Ultimately, the illumination power determines the sensitivity of an OCT system for a given frame rate. At the same time, power is limited by the maximum intensity that can safely illuminate the sample. Conventionally, in flying-spot OCT, a focused light beam is scanned, and the maximum power that can safely be used is determined by the focal spot size. In contrast, in parallel OCT, a line focus is applied to the sample, and all A-lines are simultaneously recorded. Distributing the illumination across a line allows for higher total power while maintaining a lower peak intensity than that of flying-spot OCT. The higher power enables higher sensitivity at a given frame rate. However, parallel OCT systems have not yet demonstrated this improved sensitivity due to lack of appropriate high-power, high-bandwidth sources.

After its invention in 1999 [4], parallel OCT has seen notable improvements in speed, sensitivity, and resolution. To the authors' knowledge, the fastest speed in a parallel SD-OCT system was achieved by Grajciar et al. at 512,000 A-scans/sec with a sensitivity of 74 dB and an axial resolution of 18 µm [5]. The highest axial resolution of a parallel SD-OCT system is 1.22 µm with a sensitivity of 89 dB [6]. Zhang et al. [7] reported the highest sensitivity with a parallel OCT configuration (94 dB), with an axial resolution of 3 μ m and a speed of 265,000 A-lines/sec. Recent advances in commercially available supercontinuum (SC) sources to minimize relative-intensity noise have allowed them to be operated in the shot-noise limit for OCT [8,9], while offering an order-ofmagnitude increase in power as compared to traditional OCT light sources. With higher power we can achieve higher sensitivity. Such a SC source has recently been used In this Letter, we show that the use of a SC light source in combination with a parallel SD-OCT configuration offers higher sensitivity and higher frame rate than any parallel SD-OCT system reported to date, while maintaining ultrahigh resolution. We demonstrate the utility of the system by capturing the rapidly beating cilia of human bronchial epithelial (hBE) cells *in vitro*.

Figure 1 shows the optical setup of the parallel SD-OCT system consisting of a 2D spectrometer, a free-space Michelson interferometer, and a cylindrical lens (CL). The optical paths for the two orthogonal planes of the parallel SD-OCT system after the CL, which is setup in an afocal configuration, are shown in Ref [11]. The SC source (SuperK Extreme EXR-15, NKT Photonics) has a repetition rate of 310 MHz and a wavelength range spanning 400-2400 nm. The combination of a low-pass and high-pass filter is used to narrow the spectrum, achieving a center wavelength and bandwidth of 775 and 159 nm, respectively, at the sensor. The power from the filtered SC source is 1.1 W at the input of the interferometer. The collimated light is expanded from 0.7 to 6 mm by the use of a telescope composed of lenses L0 ($f_{L0} = 35$ mm) and L1 ($f_{L1} = 300$ mm). The beam then passes through the CL ($f_{CL} = 100$ mm) before entering the 4f interferometer with achromatic lenses L2, L3, and L4 ($f_{L2} = f_{L3} = f_{L4} = 100$ mm). Because the system operates in an afocal mode, the beam after L4 is focused into a vertical line with a beam diameter of 6 mm in the vertical direction and a focused spot size of 17 µm in the horizontal direction at the sample position. The total power at the sample is 492 mW, with a power per A-line of 0.48 mW. Note that a neutral density filter (NDF) inserted into the reference arm is used to adjust the power, so that the recorded interferogram is close to the saturation level of the sensor. At the same time, a matched NDF in the sample arm balances interferometer dispersion; it is normally set to no attenuation except when imaging a mirror to characterize resolution and SNR.



Fig. 1. Illustration of the parallel SD-OCT system (horizontal plane shown; see Ref. [11] for the vertical plane). M, mirror; NDF, neutral density filter; L, lens; BS, beam splitter. Panels (a) and (b) plot the spectrum and the transverse intensity distribution of the beam, respectively, both at the sensor plane with the sample arm blocked.

The backscattered light from both arms are recombined at the exit of the interferometer and detected by the spectrometer. The beam is reduced to the size of the sensor by L5 $(f_{L5} = 200 \text{ mm})$ and L6 $(f_{L6} = 50 \text{ mm})$. The spectrometer is composed of a diffraction grating (DG; 600 lp/mm, Wasatch Photonics) set at its Littrow angle, an achromatic lens $(f_{L7} = 100 \text{ mm})$, and a high-speed 2D CMOS camera (FastCam SA3, Photron) placed at the back-focal plane of L7. The sample and camera planes are conjugated so that each row of the 2D CMOS array is associated with a different transverse position of the sample. The transverse field of view imaged by our system is 4.15 mm. The camera $(1024 \times 1024 \text{ pixels}, 17 \text{ }\mu\text{m} \times 17 \text{ }\mu\text{m} \text{ each})$ converts the optical signals into 12-bit numerical values at a maximum frame rate of 1 kHz with a continuous acquisition time of 1.36 s. This corresponds to an imaging speed of 1,024,000 A-scan/s used for all images in this study, which is, to our knowledge, higher than that of any previously reported parallel SD-OCT systems. We note that in this demonstration we are oversampling in the transverse direction, whereas flying-spot OCT systems can readily adjust the rate of transverse sampling. B-mode OCT images are reconstructed by subtracting the reference spectrum, digitally compensating for dispersion mismatches between the sample and reference arms using parameters predetermined from an iterative method [12], and computing the Fourier transform along the spectral dimension of the recorded 2D interferogram.

The SNR is measured versus depth by recording spectral interferograms of a silver mirror at different axial positions (top right panel of Fig. 2). SNR is determined from the B-mode image by the ratio between the maximum value within the center A-line and the standard deviation of the noise immediately surrounding the peak. The optical attenuation of a double pass through the NDF in the sample arm (73 dB) is then added back. Operating in the shot-noise limit as characterized by Ref [9], the maximum SNR is thus found to be 113 ± 2 dB at a depth of 100 µm, rolling off to 90 dB at a depth of 350 µm. This roll-off is consistent with a spectral resolution of 67 µm, is associated with the limited *f*-number of the imaging lens in our spectrometer [13], and could be improved



Fig. 2. Experimental evaluation of the parallel SD-OCT system. Top panels plot the measured axial response and SNR of a mirror at different depths. Bottom panel shows the reconstructed B-mode image of point-like scatterers. The insets show two point-like scatterers and their experimentally determined lateral and axial resolutions.

with redesign. To estimate the theoretical SNR, we use the same expression as in flying-spot SD-OCT [14]. However, we use the average power per A-line and then add back the 3 dB difference between the average power and the maximum power at the center A-line. In this way, the theoretical SNR is found to be 122 dB for an exposure time of 1 ms. Considering optical losses of 8 dB between the sample and detector planes, these theoretical and experimental sensitivities are in good agreement. To our knowledge, our experimental SNR of 113 dB is higher than that of the previously fastest parallel SD-OCT system (0.5 million lines/s, SNR of 78 dB) [5], and of the fastest flying-spot SD-OCT system (1 million lines/s, sensitivity of 71 dB) [3]. We also note that a parallel SS-OCT system was recently reported at 1 MHz line rate offering 90 dB [15].

As in flying-spot SD-OCT, the axial resolution (Δz) is determined by the spectral bandwidth and the center wavelength. Given the spectrum of our system, the theoretical axial resolution is 1.8 μ m in air. Experimentally, Δz is measured as a function of depth from the full width at half-maximum (FWHM) of a silver mirror (top left panel of Fig. 2). We obtain $\Delta z = 2.0 \pm 0.2 \ \mu$ m, which is in agreement with the theoretical resolution. It is interesting to note that in parallel SD-OCT, the in-plane lateral resolution (Δx) is dictated by the limiting aperture within the collection optics (L4-L7 and DG), while the out-of-plane lateral resolution (Δy) is given by the illumination linewidth on the sample (after verifying that the beam width reflected from the sample is not clipped by the collection optics). This corresponds to Δy equal to the line focus width of 17 µm, while Δx is expected to be ≤ 17 µm. To measure Δx , we image a transparent silicone sample containing a sparse distribution of point-like scatterers comprised of TiO₂ powder (mean diameter <5 µm, Part No. 224227, Sigma Aldrich), as shown in Fig. 2. Twenty intense, point-like scatterers were selected at various depths, for which the FWHM of the transverse and axial profiles were determined. By averaging the results, we find $\Delta x = 14 \pm 3 \,\mu\text{m}$ and $\Delta z = 1.8 \pm 0.4 \,\mu\text{m}$, both of which are consistent with theory.

The advantages of the combination high speed and high sensitivity of SC-based parallel OCT are demonstrated by imaging an hBE culture to capture the rapid motion of cilia. Mucus provides a first line of defense against infection by trapping inhaled pathogens in our airways. Beating cilia propel mucus to the esophagus which expels pathogens from the airway. Airway diseases such as COPD are characterized by a breakdown of mucociliary clearance resulting in chronic lung infections. It is therefore beneficial to be able to assess ciliary activity at the respiratory epithelium. Previously, the beating of a single cilium tip has been tracked using a micro-OCT system with 1 µm axial resolution to make a direct measure of ciliary beat frequency (CBF) [2]. Although our parallel SD-OCT is not capable of spatially resolving individual cilia, it is fast enough to detect the rapid speckle fluctuations of beating cilia, which were previously described in Ref. [16]. Importantly, the quantitative measures of ciliary activity in [2,16] were limited to individual A-lines in time (M-mode), while the use of parallel OCT in this study enables assessment of ciliary dynamics over the entire B-mode frame.

In this study, well-differentiated cultures of hBE cells demonstrating mucociliary transport are prepared as previously described [17,18]. Briefly, primary human airway epithelial cells are isolated from excess tissue by the University of North Carolina (UNC) Tissue Procurement and Cell Culture Core under protocols approved by the UNC Institutional Review Board. Then, cells are plated on collagen-coated membranes (MilliCell, Millipore, PICM03050, $0.4 \mu m$, 30 mm diameter) and cultured at the air/liquid interface (ALI) using established protocols [17,18]. The cells form a pseudostratified mucociliary epithelium with abundant cilia at an ALI. Note that, in these studies, the culture insert is modified to create a circular track allowing mucus to be transported in a continuous circular path [19] [Fig. 3(a)]. Cultures are examined by conventional wide-field microscopy, and those that have fully developed cilia and show continuous mucus transport are imaged.

We first compare a static B-mode image [Fig. 3(b)] with the known structure of the hBE cell culture [Fig. 3(a)]. From the static image, only the membrane, air, and media regions are clearly distinguishable; it is not possible to distinguish the hBE cells, the periciliary layer (PCL), or the mucus. However, regions of rapid ciliary activity become apparent in Visualization 1 generated from successive B-mode frames. To quantify the dynamic information, we analyzed the speckle fluctuation spectrum at each pixel. Example fluctuation spectra are displayed for a single column of data from an M-mode image [Fig. 3(c)]. In these data, the PCL is attributed to a rapidly fluctuating layer with high-frequency components (yellow arrow and bracket), the membrane is attributed to a highly scattering, stationary layer (purple bracket), and the hBE cells are in between (green bracket). These layers are also apparent in the full cross-sectional view in Visualization 1.

Respiratory epithelial cilia are known to beat in a timeharmonic way with a distinct CBF. However, the power spectrum of the resulting OCT signal amplitude is expected to contain frequency components much larger than CBF, because (1) the ciliary motion is not generally sinusoidal, and (2) amplitude and phase modulation results in further nonlinearity in the OCT signal amplitude. It was previously shown that the median frequency (fm) of the speckle fluctuation



Fig. 3. Parallel SD-OCT of an *in vitro* ALI hBE culture. (a) Sketch of an hBE culture cross section (top) and diagram of imaging geometry (bottom). (b) B-mode OCT image of a single frame (see Visualization 1 for video at 0.4× real time). Arrows indicate features color matched to those in panel (a). (c) M-mode image reconstructed from one A-line of the B-mode stack and its corresponding Fourier spectrum. The depth of the M-mode and spectrum image spans from 103 to 247 μ m.

spectrum, which is posited to be directly proportional to the CBF, is correlated with changes in ciliary activity under isoflurane treatment [16]. Here, we measured f_m from the fluctuation spectrum at each pixel in the B-mode image by omitting the DC term and subtracting white noise (which was estimated as the average over the 300–500 Hz band). Because f_m in regions of low scattering can be large, a method for automatically segmenting the f_m map was developed to select only features with significant fluctuation amplitude. This method involves thresholding based upon the area under the curve of the fluctuation spectrum (after omitting DC and subtracting white noise). Since this value is, on average, two orders of magnitude lower in regions outside the cell culture than inside the culture, by setting a threshold on this value, the f_m map is automatically segmented.

Figure 4(a) shows the f_m map overlaid in rainbow hue on the same B-mode image from Fig. 3(b) of the in vitro hBE cell culture. Importantly, from this f_m map one can now distinguish between the PCL and the hBE cells, where f_m is a semiquantitative measure of ciliary activity. In fact, the PCL shows up distinctly as a thin layer on the upper border of the hBE cells. Note that this image does not show a mucus layer because the hBE culture has been washed to remove any thick, turbid mucus. Next, dynamic imaging of hBE cells with endogenous mucus is performed (see Visualization 2). Rather than a monolayer of cells [as in Fig. 4(a)], the area of the culture imaged in Fig. 4(b) has a more complex structure. However, the f_m analysis still produces images that selectively contrast ciliary activity and enables identification of the PCL, as indicated by the yellow arrow. For both cultures of Fig. 4, the ciliary activity is characterized by $f_{\rm m}$ of ~50–80 Hz. This is larger than the actual CBF, but is known to change proportionally with changes in CBF [16].

In summary, a broadband SC source has been implemented in a parallel SD-OCT system. The main advantages of this source are its wide spectral bandwidth providing ultrahighresolution images (axial resolution of $2 \mu m$), and its high optical

Median-frequency map

Fig. 4. Dynamic OCT imaging using the median-frequency map (f_m) for two hBE cultures (a) without mucus and (b) with mucus (see Visualization 2 for video of B-mode OCT images at 0.4× real time). Colored arrows indicate the different layers of the culture.

power, which results in high-sensitivity images (maximum SNR of 113 dB). Importantly, the parallel SD-OCT geometry takes advantage of this increase of optical power by distributing it across a line focus. We have not observed any change in f_m by potential photothermal heating after >2 min of continuous exposure, however, further investigation into heating in the line-focus geometry is needed before use *in vivo*. The combination of this SC source with a high-speed camera in a parallel OCT configuration now enables kHz frame rates (with effective MHz line rates) with a competitive imaging performance compared with commercial SD-OCT systems. This will enable new applications in studying dynamics of highly transient effects such as chemical reactions and biological motility.

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